

# Quantifying and analysing the variability of PV module resistances $R_{SC}$ and $R_{OC}$ to understand and optimise kWh/kWp modelling

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## 1) Introduction

- The IEC 61853-1 matrix method characterises PV module efficiency vs. irradiance ( $G_I$ ) and module temperature ( $T_{MOD}$ )
- Analysing IV curves to find  $I_{SC}$ ,  $V_{OC}$ ,  $I_{MP}$ ,  $V_{MP}$ ,  $R_{SC}$  and  $R_{OC}$  gives more useful information than just efficiency measurements at  $V_{MP}$
- Combining Loss Factor Model (LFM) type analysis of IV curves with IEC 61853-1 matrices gives best understanding.

## 2) Fitting IEC 61853-1 performance vs. $G_I$ and $T_{MOD}$

The Mechanistic Performance Model (MPM) fits  $PR_{DC}$  for both indoor and outdoor matrix measurements [1].

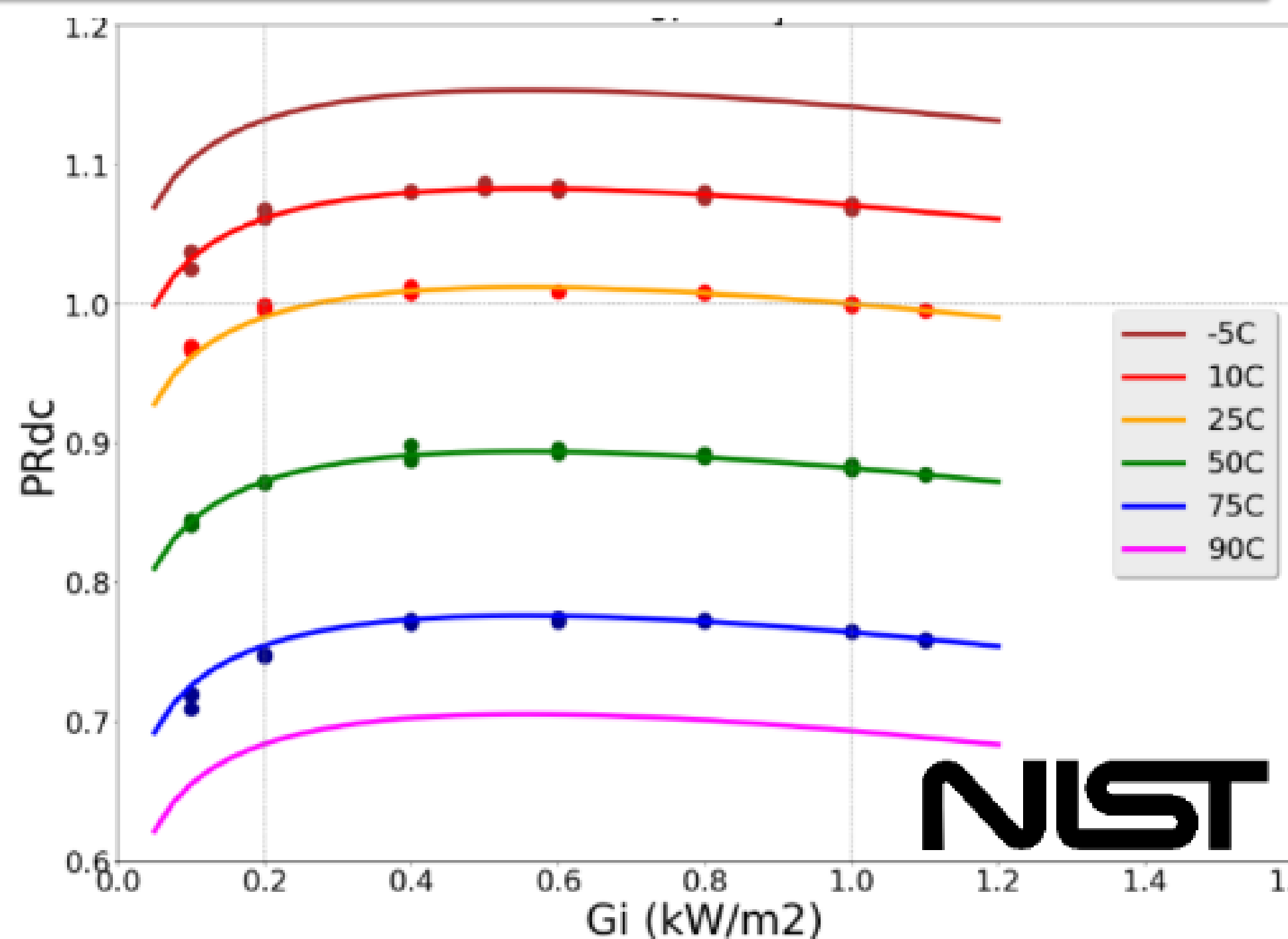
MPM has 6 meaningful, orthogonal, normalised and robust coefficients (for simplicity only  $C_1$  to  $C_4$  are used here)

$$PR_{DC} = C_1 + C_2 \times dT_{MOD} + C_3 \times \log_{10}(G_I) + C_4 \times G_I + C_5 \times WS + C_6/G_I$$

Typical indoor IEC 61853-1 data

Measured : points  
MPM fit : lines  
RMS fit error <0.2%

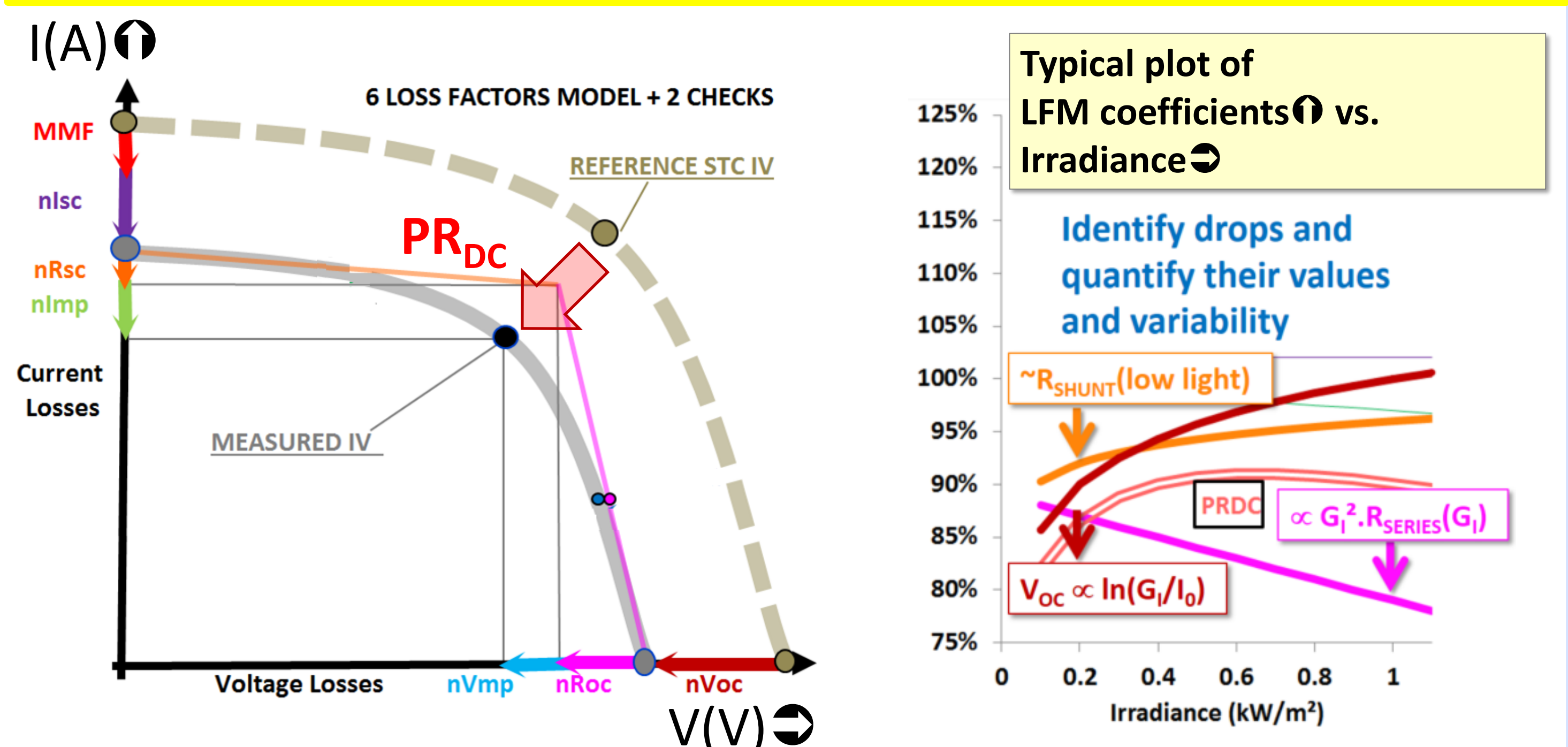
(NIST/CFV data)



## 3) Characterising IV curves with the Loss Factors Model

LFM has 6 meaningful, orthogonal, normalised parameters [2] (spectral module mismatch factor MMF not used here)

$$PR_{DC} = [nI_{SC} \times nR_{SC} \times nI_{MP}] \times [nV_{MP} \times nR_{OC} \times nV_{OC}]$$



LFM values vs. irradiance show efficiency is affected by  
Low irradiance :  $nR_{SC}$  (dominated by  $R_{SHUNT}$ ) and  $nV_{OC,T}$   
High irradiance :  $nR_{OC}$  (dominated by  $R_{SERIES}$ )

## 4) High quality IV measurements are needed for the best analysis (e.g. from GI's OTF)

[www.gantner-environment.com/products/outdoor-test-facility.html](http://www.gantner-environment.com/products/outdoor-test-facility.html) [3]



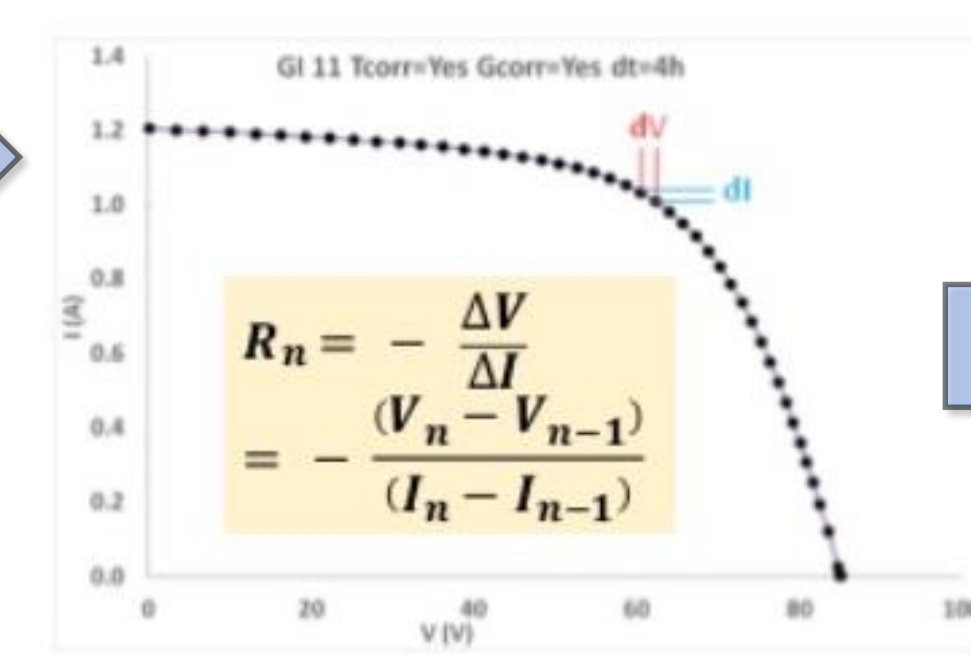
Measurement range: V: 0...60 V, I: 0 ... 50 A, Pmax: 400 W (800 W max.)  
24bit resolution (1200 VDC permanent)  
Fast & high accuracy digitalization, 50 kHz sample rate per channel, accuracy 0.01 % typical  
Fast response time: (10 ... 100%): 30us  
Dynamic sweep time and scan interval (from seconds to hours)  
On the fly calculation of all key parameters  $I_{SC}$ ,  $R_{SC}$ ,  $I_{MP}$ ,  $V_{MP}$ ,  $R_{OC}$ ,  $V_{OC}$ ;  
Real time performance prediction  
Optional outdoor spectroradiometer  
Reliable and proven industry components and calibrated sensors

GI OTF  
(Shown in AZ)

Smooth IV curves are needed for good  $R_{SC}$  and  $R_{OC}$  calculations

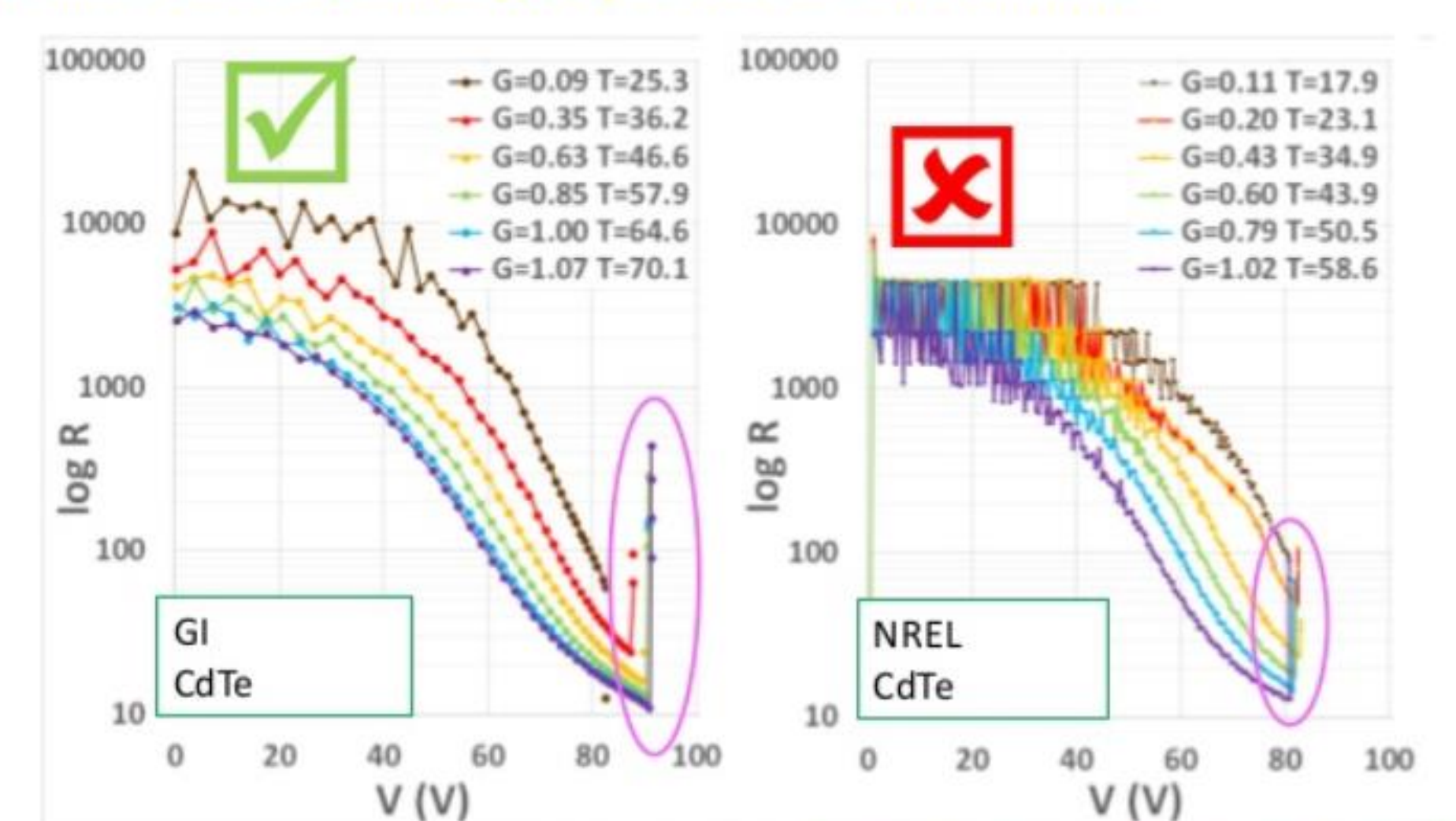
Typical GI measured IV curve (CdTe)

" $R_n$  = Apparent resistance between adjacent data points"



Note : Smooth IV curves result in most accurate analysis

Checking IV data quality with Log Resistance-Voltage (RV) curves  
GI data much smoother than NREL's Daystar and therefore easier to fit.



Can ignore a few "bad end points" with  $V=0$  or  $V > V_{OC}$

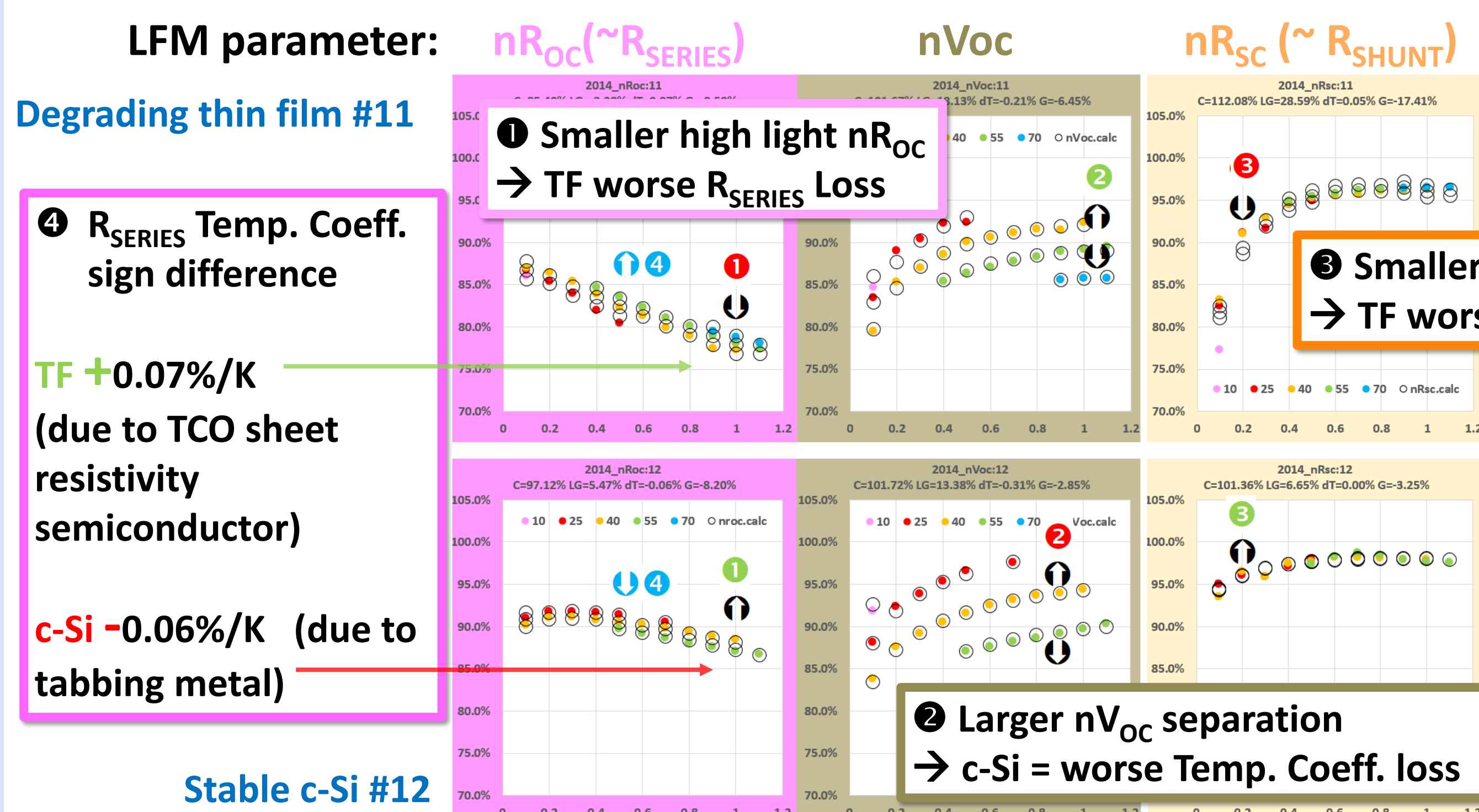
## 5) Optimum performance analysis with LFM coefficients, MPM model and IEC 61853-1 matrix data

Fit all 6 LFM parameters with MPM type equations using matrix approach of  $G_I$  and  $T_{MOD}$  bins for each year

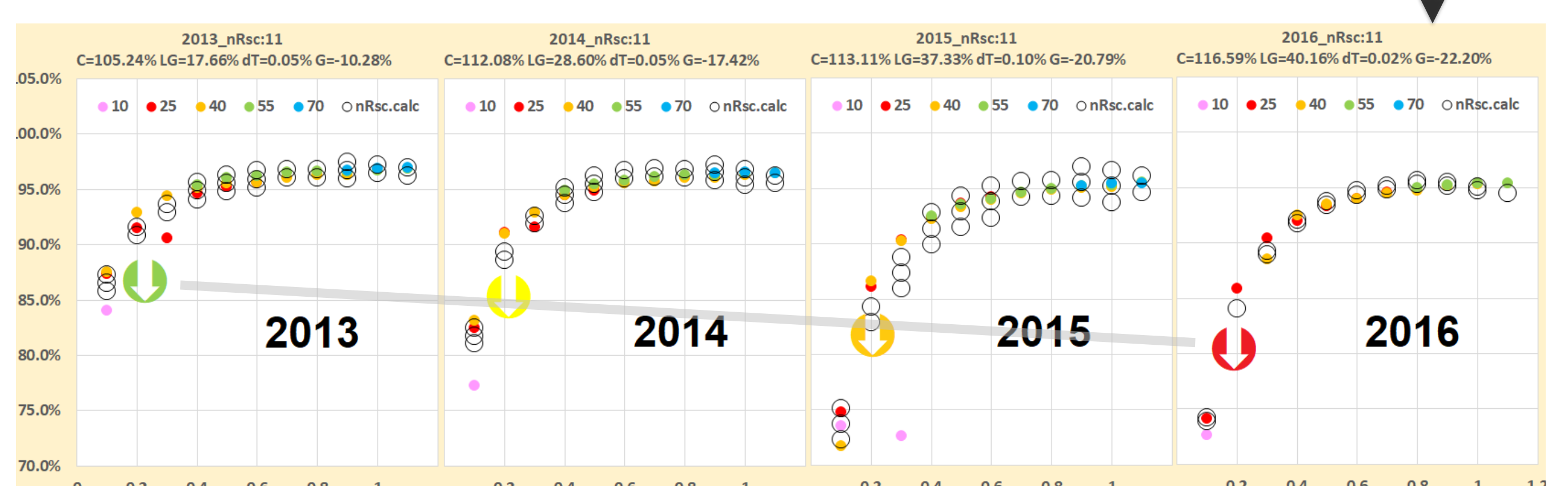
$$nLFM = C_{LFM1} + C_{LFM2} \times dT_{MOD} + C_{LFM3} \times \log_{10}(G_I) + C_{LFM4} \times G_I \quad \text{<LFM/MPM>}$$

Comparing 3 LFM parameters  $nR_{OC}$  vs.  $G_I$  and  $T_{MOD}$  (coloured dots) for two technologies (GI measurements, 2014)

KEY TO LEGEND :  
YEAR LFM\_PARAMETER MODID  
Coefficients  
1 C = constant (quality %)  
2 dT = delta Tmod Temp Coeff (%/K)  
3 LG = log10Irrad (low light %)  
4 G = GI (high light %)



$nR_{SC}$  vs.  $G_I$  : Finding the cause and rate of drop of a degrading module 2013-16 (GI Measurements)



7% Performance fall at low light in 3 years is caused by degrading  $R_{SHUNT}$  causing  $nR_{SC}$  to reduce (Gantner Instruments data)  
As  $PR_{DC}$  is the product of six coefficients –  
any drop or change has a direct influence on  $PR_{DC}$  and therefore energy yield.

## 6) Glossary + references

LFM	Loss Factors Model [2]
MPM	Mechanised Performance model [1]
$G_I$	Plane of array instantaneous irradiance (kW/m <sup>2</sup> )
$T_{MOD}$	Module Temperature (C)
$dT_{MOD}$	Module temperature rise - 25 (C)
OTF	Outdoor Test facility as sold by Gantner Instruments
STC	Standard Test Conditions 1kW/m <sup>2</sup> , 25C $T_{MODULE}$ , AM1.5, 0 ms <sup>-1</sup>
LLEC	"Low light efficiency coefficient" = $(Eff_{0.2kW/m^2} / Eff_{1kW/m^2})$
NOCT	$T_{MODULE}$ @ (0.8kW/m <sup>2</sup> , 20C $T_{AMBIENT}$ , AM1.5, 1ms <sup>-1</sup> )
$I^2Rs$	% Loss in series resistance = $I_{MAX}^2 \times R_{SERIES} / P_{MAX,STC}$
nLFM	normalised LFM coefficient
nLFM_T	Temperature corrected LFM coefficient

[1] MPM (papers 79, 81, 82) [steve@steveransome.com](mailto:steve@steveransome.com)  
[2] LFM (paper 70) [steve@steveransome.com](mailto:steve@steveransome.com)

## 7) Conclusions

- The causes and rates of PV performance degradation (e.g. " $R_{SHUNT}$  at low light") can easily be found using these methods with high quality IV data such as from GI's OTF
- Optimized MPM curve fitting has been generalised and combined with the LFM
- MPM coefficients give normalized values for quality, temperature dependence, low light (due to  $V_{OC}(G_I)$  and  $R_{SHUNT}(G_I)$ ) and high light drops due to  $I^2.R_{SERIES}$

[3] Gantner Instruments [www.gantner-environment.com/products/gantnerwebportal.html](http://www.gantner-environment.com/products/gantnerwebportal.html)